

# Modeling of Soil Carbonation for sustainable soil subgrade stabilization.

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## Motivation

- Collapse in subgrade soils due to Freeze-Thaw.
- Conventional stabilizing agents have a large carbon footprint (approximately 1 ton of carbon dioxide (CO<sub>2</sub>) gas per ton of cement (UNEP-GEAS, 2010) or lime (Stork et al., 2014) production).
- One solution to increase strength and stiffness while reducing net CO<sub>2</sub> emissions is using carbonate binders, which consume CO<sub>2</sub> through carbonation.

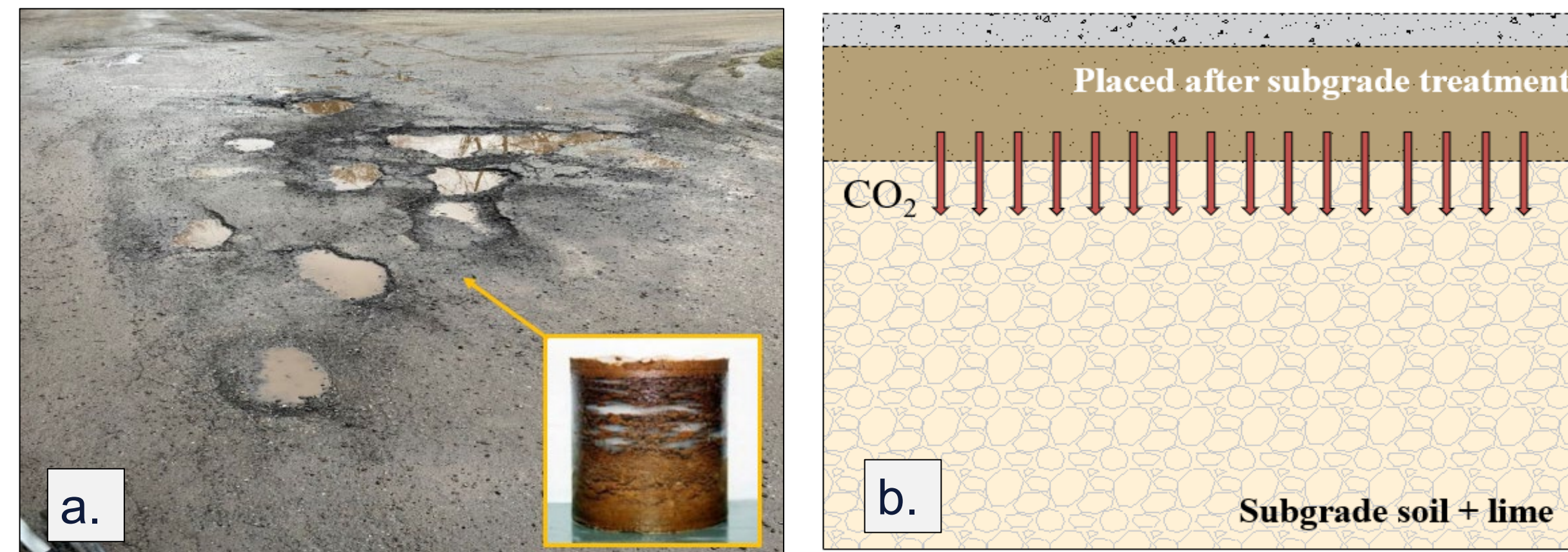


Fig. 1). a. Pavement damage due to soil frosting.  
b. Potential solution with Soil Carbonation

## How does it work?

- The CO<sub>2</sub> reacts with the lime (at controlled saturation conditions)
- This reaction creates stable carbonate minerals (binder) that attach the particles.
- Increase in the strength and stiffness of soil

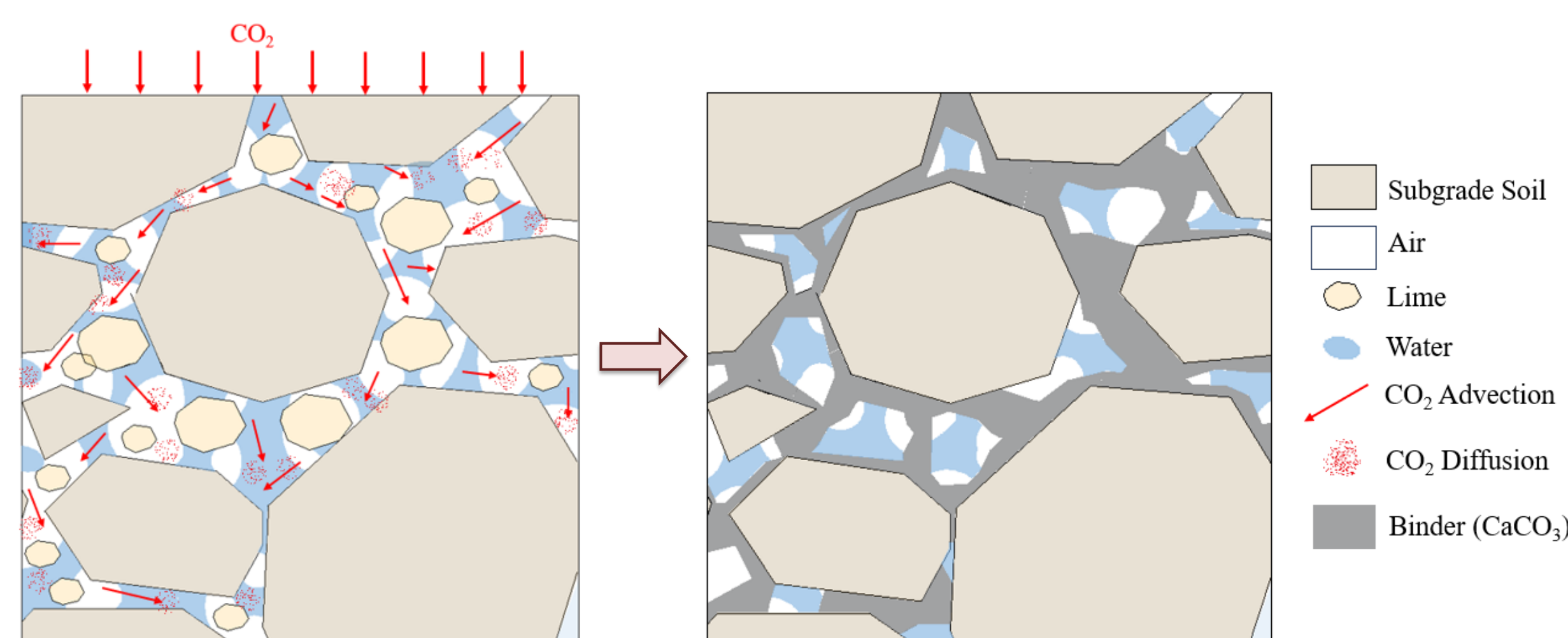
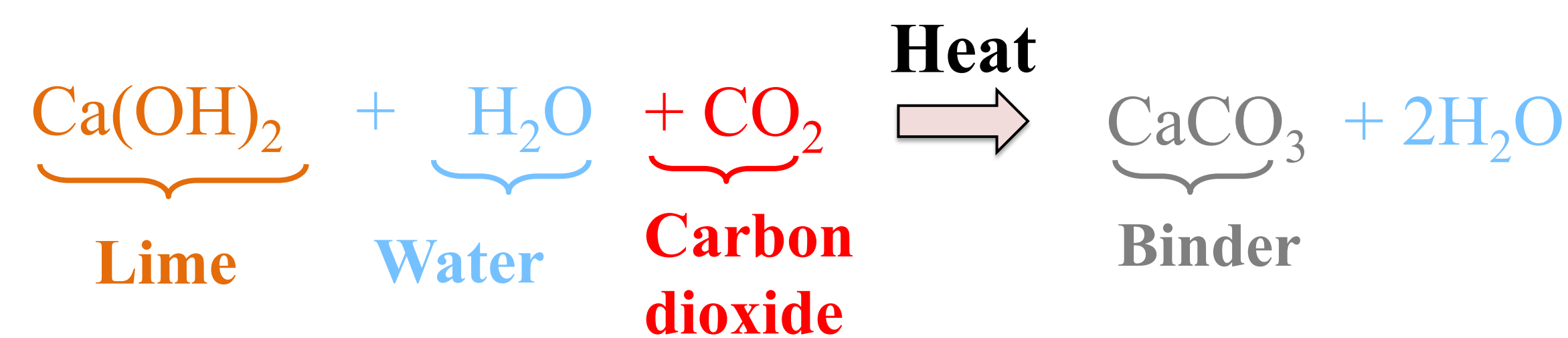


Fig. 2). Microstructure of the soil fabric during carbonation

## Modeling Soil Carbonation

**Step 1. Gas Transport in Porous Media** (No reaction included)  
Discretization using **Finite Element Analysis (FEA)** for multigas transport was done using Mass Conservation combined with Darcy's and Fick's law for advective and diffusive flow, respectively.

$$\mathbf{M} \left[ \frac{\partial(\theta \vec{c}^i)_k}{\partial t} \right] = -\mathbf{K}_{ad}^i \left( \sum_{j=1}^N \vec{c}_k^j \right) - \mathbf{K}_{diff} \left( \sum_{j=1}^N D_{ij} \vec{c}_k^j \right) + \vec{q}$$

Change in Concentration
Flow Advection
Flow Diffusion
Output/Input Flow

**Model Validation:** from Ogata and Banks (1961) analytical solutions

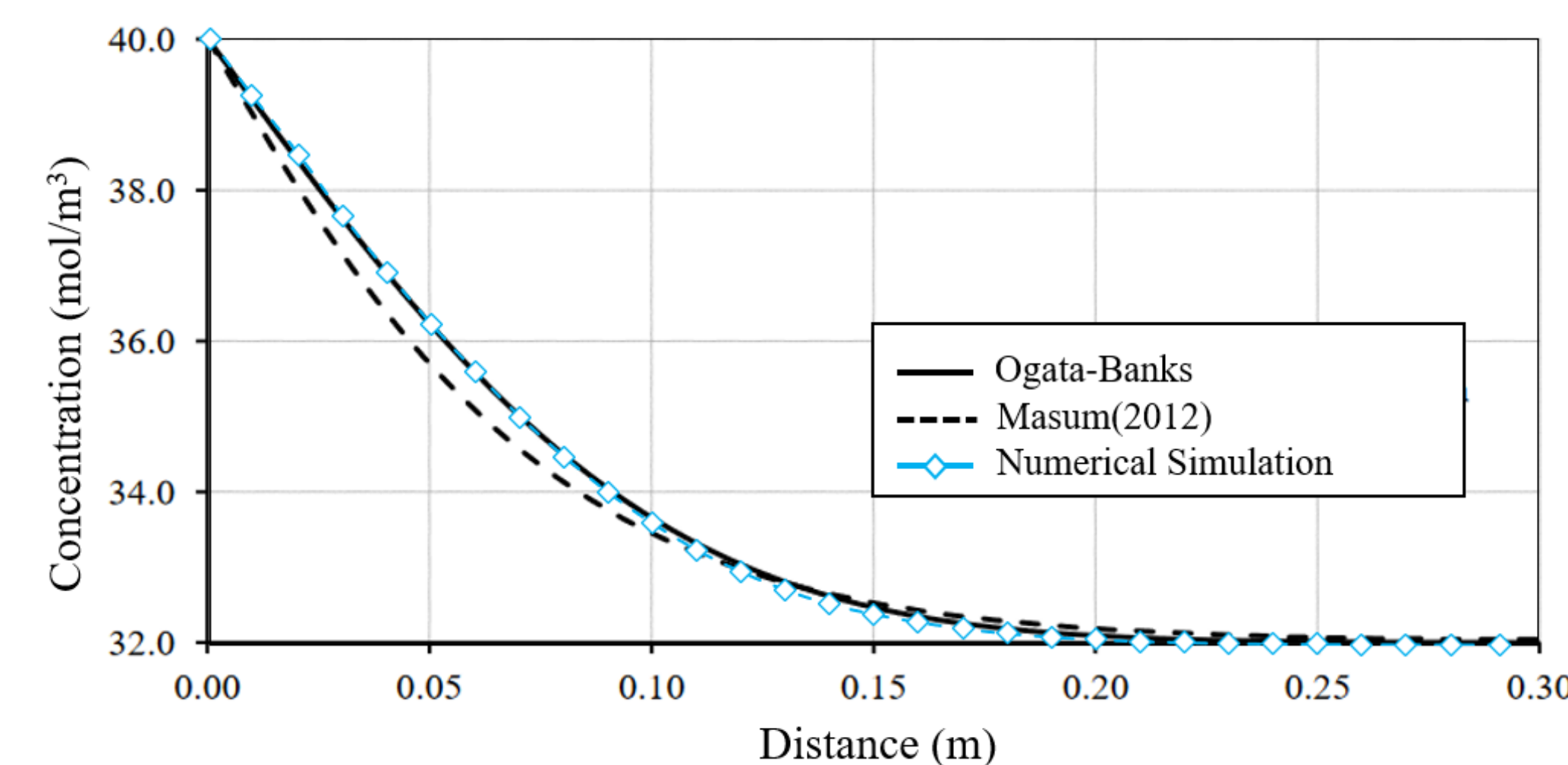


Fig 3). Comparison between Ogata-Banks(1961) analytical solution, Mason' (2012) numerical model, and the current numerical simulation for an advection-diffusion problem

## Step 2. Including Carbonation Reaction :

**Carbonation:** Represents the consumption of CO<sub>2</sub> in the system because of the production of CaCO<sub>3</sub> (Binder)

$$\mathbf{M} \left[ \frac{\partial(\theta \vec{c}^i)_k}{\partial t} + \frac{\partial(\theta_g \vec{S}_g^i)_k}{\partial t} \right] = -\mathbf{K}_{ad}^i \left( \sum_{j=1}^N \vec{c}_k^j \right) - \mathbf{K}_{diff} \left( \sum_{j=1}^N D_{ij} \vec{c}_k^j \right) + \vec{q}$$

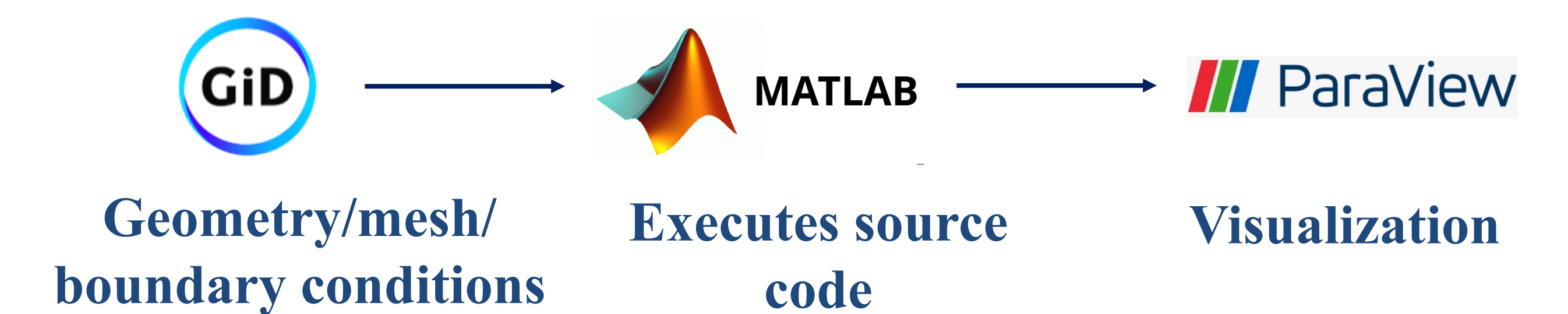
**Carbonation / (Sink term)**

The rate of CaCO<sub>3</sub> production from the reaction of CO<sub>2</sub> with Ca(OH)<sub>2</sub> is based on Papadakis et al., 1991:

$$S_{CaCO_3} = K_i \times [Ca(OH)_2] \times [\theta_w] \times [CO_2]$$

**Coefficient of the carbonation reaction**
**Volumetric water content [-]**

## FEM features / preliminary results



Simulation of a one-dimensional carbonation test:

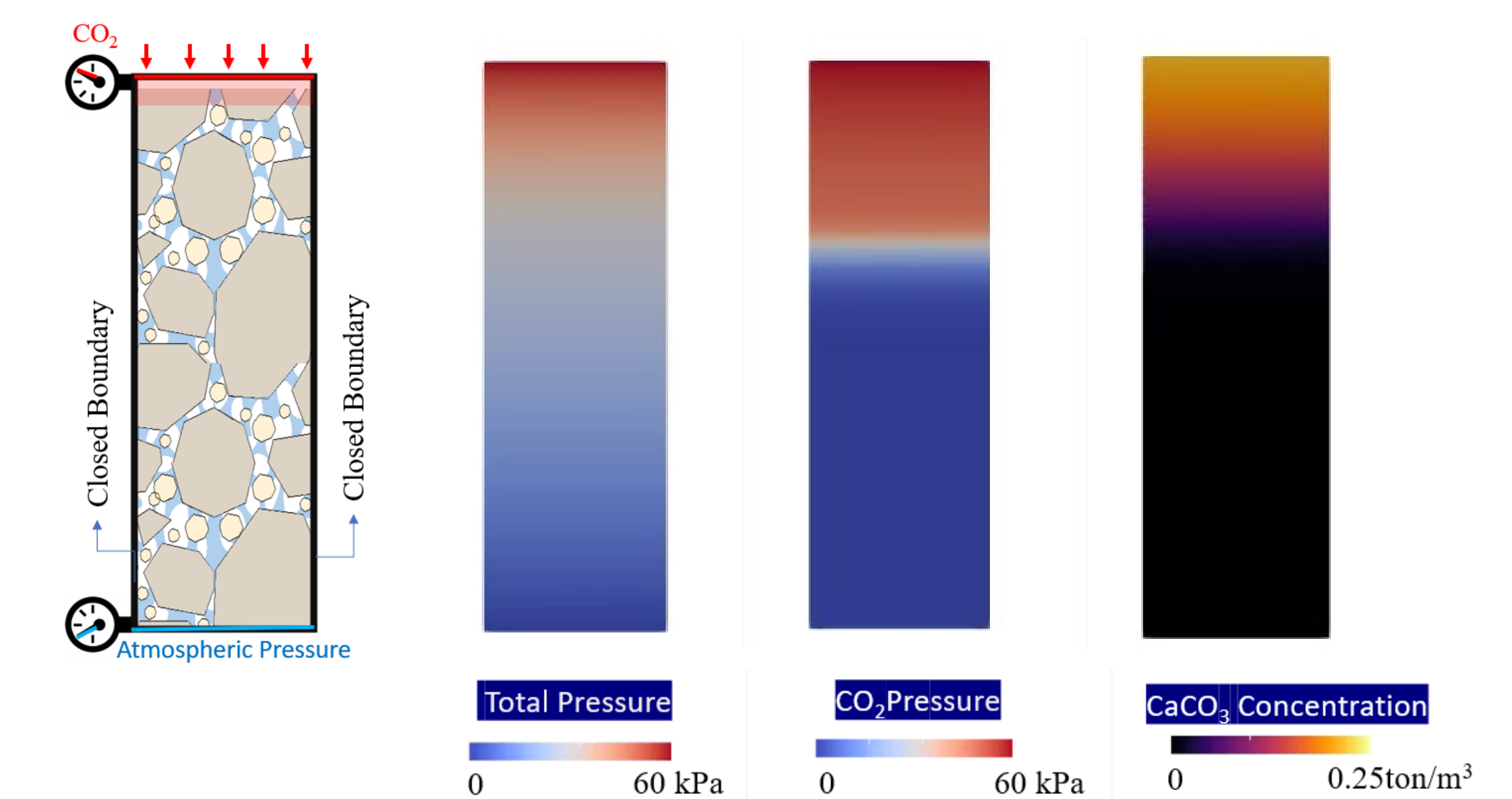


Fig 4). One-dimensional carbonation simulation

## Laboratory work for calibration

Need to calibrate K<sub>i</sub> (Coefficient of the carbonation) from laboratory results

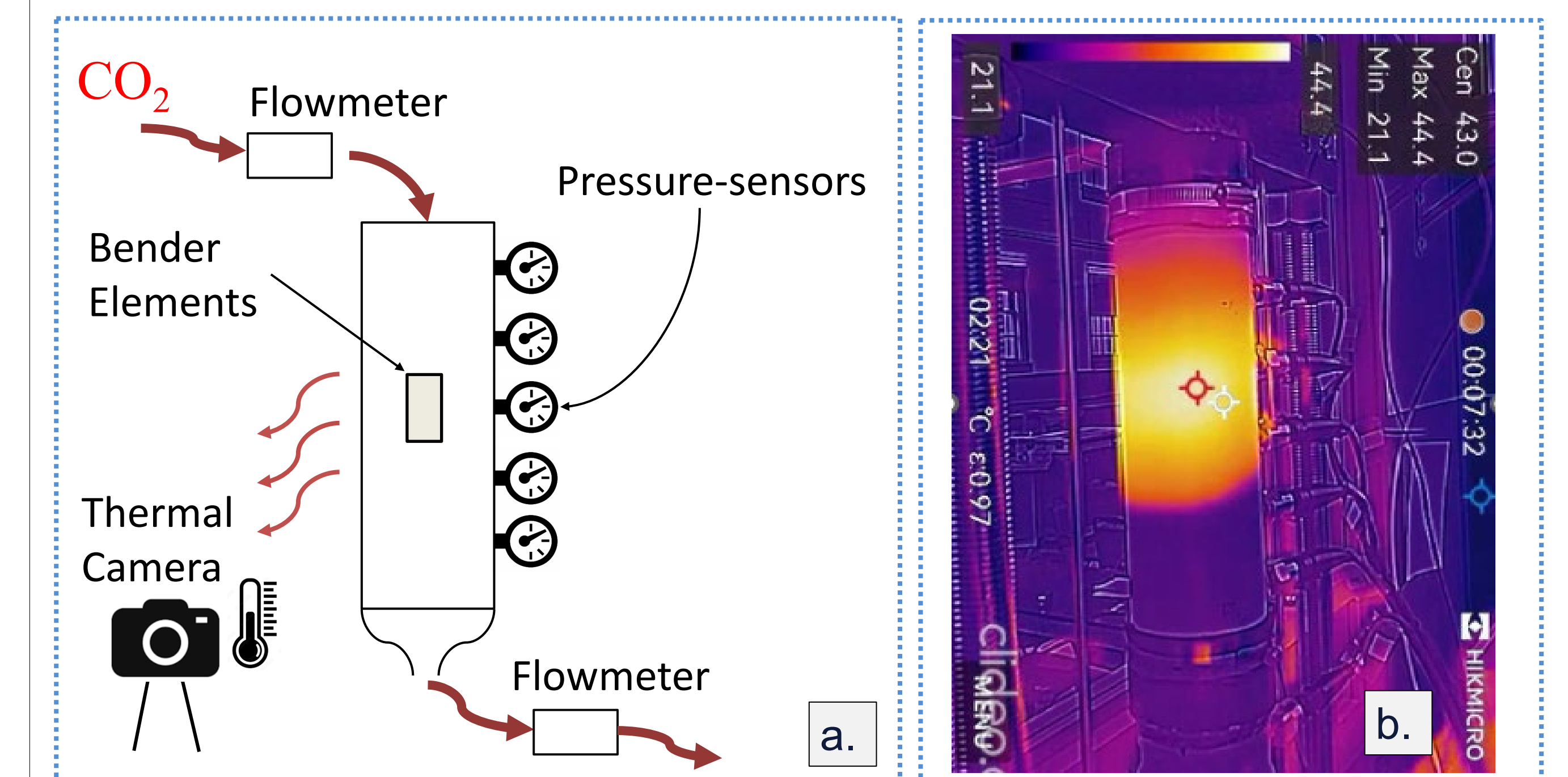


Fig 5). Laboratory setup – b. Thermal Camera capturing carbonation

## Future work

- Parametric study for calibration of the carbonation reaction based on the laboratory results.